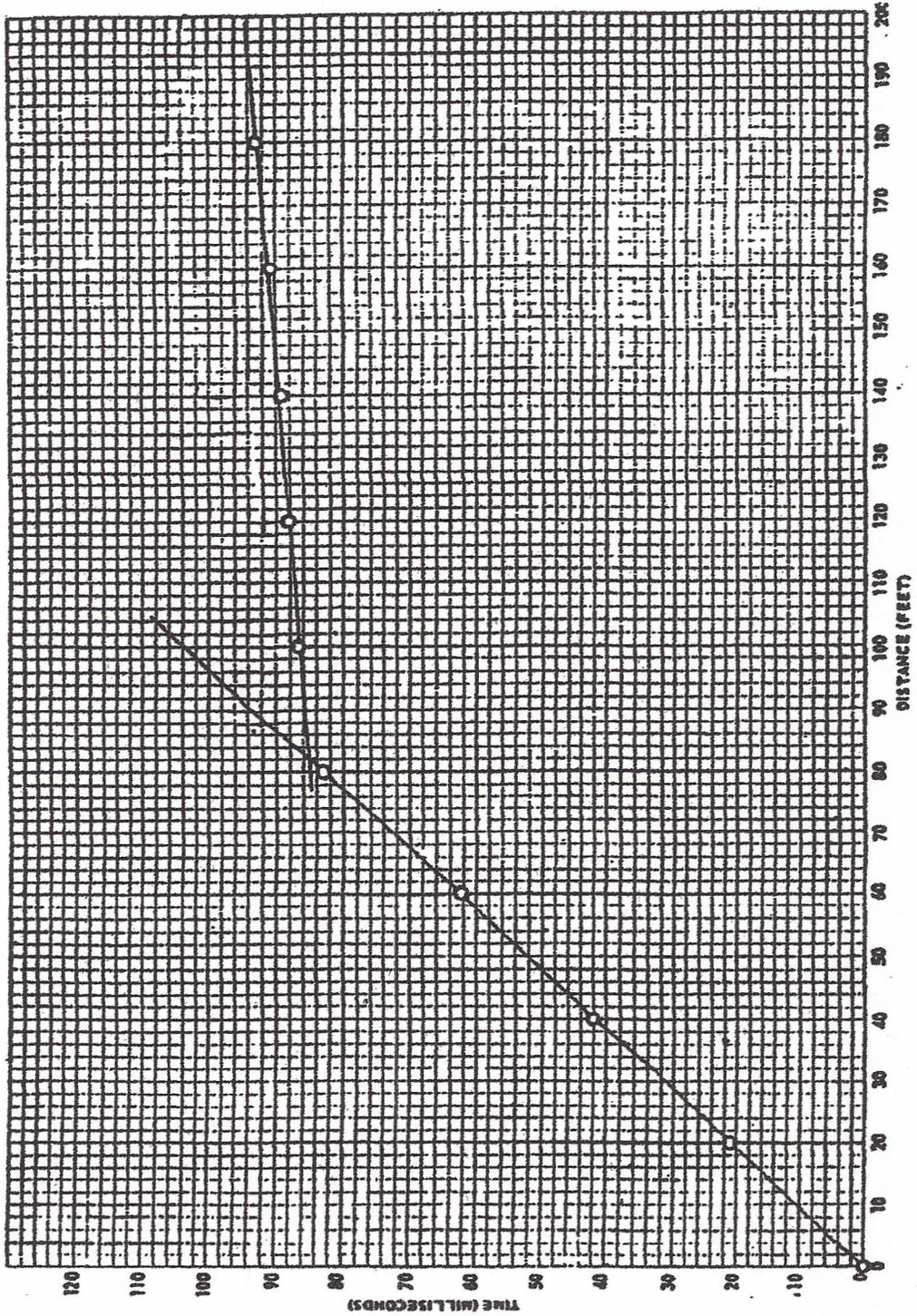


CHAPTER 3

- (3-1) (a) $p_0 = (10)(120)/2000 = 0.600 \text{ ton/ft}^2$
 Eq. (3-1): $C_N = 0.77 \log_{10} (20/0.600) = 1.17$
 $N_{\text{corrected}} = (1.17)(26) = 30$
 (b) $10 \text{ ft} = 3.048 \text{ m}$ and $120 \text{ lb/ft}^3 = 18.85 \text{ kN/m}^3$
 $p_0 = (3.048)(18.85) = 57.45 \text{ kN/m}^2$
 Eq. (3-3): $N_{\text{corrected}} = (26)(100/57.45)^{1/2} = 34$
- (3-2) (a) $p_0 = [(8)(120) + (2)(120 - 62.4)]/2000 = 0.538 \text{ ton/ft}^2$
 Eq. (3-1): $C_N = 0.77 \log_{10} (20/0.538) = 1.21$
 $N_{\text{corrected}} = (1.21)(26) = 31$
 (b) $p_0 = 1.08 \text{ kips/ft}^2 = 51.71 \text{ kN/m}^2$
 Eq. (3-3): $N_{\text{corrected}} = (26)(100/51.71)^{1/2} = 36$
- (3-3) (a) $p_0 = (7)(20.40) = 142.8 \text{ kN/m}^2$
 Eq. (3-2): $C_N = 0.77 \log_{10} (1915/142.8) = 0.868$
 $N_{\text{corrected}} = (0.868)(22) = 19$
 (b) Eq. (3-3): $N_{\text{corrected}} = (22)(100/142.8)^{1/2} = 18$
- (3-4) (a) $p_0 = (2)(20.40) + (5)(20.40 - 9.81) = 93.75 \text{ kN/m}^2$
 Eq. (3-2): $C_N = 0.77 \log_{10} (1915/93.75) = 1.01$
 $N_{\text{corrected}} = (1.01)(22) = 22$
 (b) Eq. (3-3): $N_{\text{corrected}} = (22)(100/93.75)^{1/2} = 23$
- (3-5) Eq. (3-4): $c = 61/\{(\pi)[(4/12)^2(8/12)(1/2) + (4/12)^3(1/6)]\} = 449 \text{ lb/ft}^2$
 From Fig. 3-17 with $PI = 40\%$, $\mu = 0.85$. Hence, $c_{\text{corrected}} = (0.85)(449) = 382 \text{ lb/ft}^2$
- (3-6) A plot of time versus distance is given on page 8.
 $\text{slope}_{\text{line 1}} = 0.083/80 = 0.001038$
 $\text{slope}_{\text{line 2}} = (0.093 - 0.08675)/(180 - 100) = 0.00007813$
 $v_1 = \text{reciprocal of slope}_{\text{line 1}} = 1/0.001038 = 963 \text{ ft/sec}$
 $v_2 = \text{reciprocal of slope}_{\text{line 2}} = 1/0.00007813 = 12,800 \text{ ft/sec}$
 $L = 82 \text{ ft}$ (from plot on page 8)
 Eq. (3-6): $H_1 = (82/2)[(12,800 - 963)/(12,800 + 963)]^{1/2} = 38 \text{ ft}$
 With $v_1 = 963 \text{ ft/sec}$, according to Table 3-3, the subsurface material in the first layer is estimated to be normal sand or loose sand above the water table. With $v_2 = 12,800 \text{ ft/sec}$, according to Table 3-3, the subsurface material in the second layer is estimated to be hard limestone, basalt, granite, or unweathered gneiss.

(3-7)

Electrode Spacing (ft)	Resistance (ohms)	Resistivity (ohm-ft)	Cumulative Resistivity (ohm-ft)
10	12.73	800	800
20	2.79	351	1151
30	1.46	275	1426
40	1.15	289	1715
50	1.05	330	2045
60	0.84	317	2362
70	1.21	532	2894
80	1.00	503	3397
90	0.97	549	3946
100	0.95	597	4543



Electrode spacing (column 1 in the preceding table) gives the approximate depth of subsurface material included in a given measurement. Resistivity (column 3 in the table) is computed from Eq. (3-7), where D is electrode spacing (column 1) and R is resistance (column 2). Hence, for the first row in the table,

$$\rho = (2)(\pi)(10)(12.73) = 800 \text{ ohm-ft}$$

Values in column 4 are cumulative resistivity values. A plot of electrode spacing versus cumulative resistivity is shown on page 10. From this plot, the thickness of the first soil layer is determined to be approximately 63 ft. Because the resistivity of the upper layer is in the range from 50 to 500 ohm-ft, according to Table 3-4, the subsurface material in this layer is estimated to be moist to dry silty and sandy soils. Because the resistivity of the lower layer is in the range from 500 to 1000 ohm-ft, according to Table 3-4, the subsurface material in this layer is estimated to be well-fractured to slightly fractured bedrock with moist-soil-filled cracks.

