

Problem 1.3-12

Figure P1.3-12 illustrates a plane wall. The temperature distribution in the wall is 1-D and the problem is steady state.

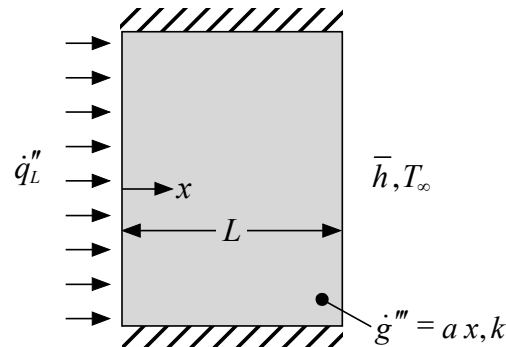


Figure P1.3-12: Plane wall.

There is generation of thermal energy in the wall. The generation per unit volume is not uniform but rather depends on position according to:

$$\dot{g}''' = a x \quad (1)$$

where a is a constant and x is position. The left side of the wall experiences a specified heat flux, \dot{q}_L'' . The right side of the wall experiences convection with heat transfer coefficient \bar{h} to fluid at temperature T_∞ . The thickness of the wall is L and the conductivity of the wall material, k , is constant.

a.) Derive the ordinary differential equation that governs this problem. Clearly show your steps.

A differential control volume is shown in Figure 2 and leads to:

$$\dot{q}_x + \dot{g} = \dot{q}_{x+dx} \quad (2)$$

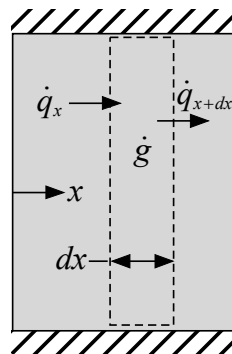


Figure 2: Differential control volume with energy terms.

After expanding the $x + dx$ term:

$$\dot{q}_x + \dot{g} = \dot{q}_x + \frac{d\dot{q}}{dx} dx \quad (3)$$

The rate of thermal energy generation within the control volume is:

$$\dot{g} = \dot{g}''' A_c dx \quad (4)$$

where A_c is the cross-sectional area of the wall. The conduction term is expressed using Fourier's law:

$$\dot{q} = -k A_c \frac{dT}{dx} \quad (5)$$

Substituting Eqs. (5) and (4) into Eq. (3) results in

$$\dot{g}''' A_c dx = \frac{d}{dx} \left(-k A_c \frac{dT}{dx} \right) dx \quad (6)$$

which can be simplified:

$$\frac{d}{dx} \left(\frac{dT}{dx} \right) = -\frac{\dot{g}'''}{k} \quad (7)$$

Substituting the position dependent generation into Eq. (7) leads to:

$$\boxed{\frac{d}{dx} \left(\frac{dT}{dx} \right) = -\frac{a x}{k}} \quad (8)$$

b.) Solve the differential equation that you obtained in (a). Your solution should include two undetermined constants.

Equation (7) is separated and integrated:

$$\int d \left(\frac{dT}{dx} \right) = \int -\frac{a x}{k} dx \quad (9)$$

which leads to:

$$\frac{dT}{dx} = -\frac{a}{2k} x^2 + C_1 \quad (10)$$

where C_1 is a constant of integration. Equation (10) is integrated again:

$$\int dT = \int \left(-\frac{a}{2k} x^2 + C_1 \right) dx \quad (11)$$

which leads to:

$$T = -\frac{a}{6k} x^3 + C_1 x + C_2 \quad (12)$$

c.) Specify the boundary conditions for the differential equation that you derived in (a).

An interface energy balance at $x = 0$ leads to:

$$\dot{q}_L'' = -k \left. \frac{dT}{dx} \right|_{x=0} \quad (13)$$

An interface energy balance at $x = L$ leads to:

$$-k \left. \frac{dT}{dx} \right|_{x=L} = \bar{h} (T_{x=L} - T_\infty) \quad (14)$$

d.) Use the results of (b) and (c) to obtain two equations that can be solved for the two undetermined constants.

Substituting Eq. (10) into Eq. (13) leads to:

$$\boxed{\dot{q}_L'' = -k C_1} \quad (15)$$

Substituting Eqs. (10) and (12) into Eq. (14) leads to:

$$\boxed{-k \left(-\frac{a}{2k} L^2 + C_1 \right) = \bar{h} \left(-\frac{a}{6k} L^3 + C_1 L + C_2 - T_\infty \right)} \quad (16)$$

Equations (15) and (16) can be solved for C_1 and C_2 .