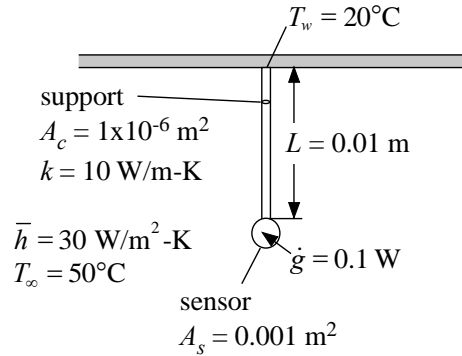


**Problem 1.2-20**

Figure P1.2-20 illustrates a temperature sensor that is mounted in a pipe and used to measure the temperature of a flow of air.

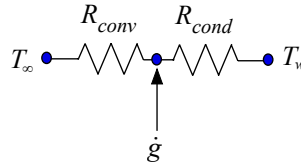


**Figure P1.2-20: Temperature sensor.**

The operation of the sensor leads to the dissipation of  $\dot{g} = 0.1$  W of electrical power. This power is either convected to the air at  $T_\infty = 50^\circ\text{C}$  or conducted along the support to the wall at  $T_w = 20^\circ\text{C}$ . Treat the support as conduction through a plane wall (i.e., neglect convection from the edges of the support). The heat transfer coefficient between the air and the sensor is  $\bar{h} = 30$  W/m<sup>2</sup>-K. The surface area of the sensor is  $A_s = 0.001$  m<sup>2</sup>. The support has cross-sectional area  $A_c = 1 \times 10^{-6}$  m<sup>2</sup>, length  $L = 0.01$  m, and conductivity  $k = 10$  W/m-K.

a.) What is the temperature of the temperature sensor?

A resistance network representation of this problem is shown in Figure 2.



**Figure 2: Resistance network.**

The resistance to conduction through the support is:

$$R_{cond} = \frac{L}{k A_c} = \frac{0.01 \text{ m}}{10 \text{ W/m-K} \cdot 1 \times 10^{-6} \text{ m}^2} = 1000 \frac{\text{K}}{\text{W}} \quad (1)$$

The resistance to convection from the sensor surface is:

$$R_{conv} = \frac{1}{\bar{h} A_s} = \frac{1 \text{ m}^2\text{-K}}{30 \text{ W/m}^2\text{-K} \cdot 0.001 \text{ m}^2} = 33.3 \frac{\text{K}}{\text{W}} \quad (2)$$

An energy balance on the sensor leads to:

$$\dot{g} = \frac{(T_s - T_\infty)}{R_{conv}} + \frac{(T_s - T_w)}{R_{cond}} \quad (3)$$

Solving for  $T_s$  leads to:

$$T_s = \frac{\dot{g} + \frac{T_\infty}{R_{conv}} + \frac{T_w}{R_{cond}}}{\frac{1}{R_{conv}} + \frac{1}{R_{cond}}} = \frac{0.1 \text{ W} + \frac{323.2 \text{ K}}{33.3 \text{ K/W}} + \frac{293.2 \text{ K}}{1000 \text{ K/W}}}{\frac{1}{33.3 \text{ K/W}} + \frac{1}{1000 \text{ K/W}}} = 325.4 \text{ K} \quad (4)$$

- b.) What is the error associated with the sensor measurement (i.e., what is the difference between the sensor and the air temperature)? Is the error primarily due to self-heating of the sensor associated with  $\dot{g}$  or due to the thermal communication between the sensor and with the wall? Justify your answer.

The error is  $T_s - T_\infty = 2.26 \text{ K}$ . The error is dominated by self-heating rather than mounting error. The mounting error would cause the sensor temperature to be less than the fluid temperature whereas the self-heating causes the temperature of the sensor to be elevated relative to the fluid temperature.

- c.) Radiation has been neglected for this problem. If the emissivity of the sensor surface is  $\varepsilon = 0.02$ , then assess whether radiation is truly negligible.

The radiation resistance is:

$$\begin{aligned} R_{rad} &= \frac{1}{A_s \varepsilon \sigma (T_s^2 + T_w^2)(T_s + T_w)} \\ &= \frac{1}{0.001 \text{ m}^2 \left| \frac{0.02}{5.67 \times 10^{-8} \text{ W}} \right| \left| \frac{\text{m}^2 \text{ K}^4}{(325.4^2 + 293.2^2)(325.4 + 293.2) \text{ K}^3} \right|} \\ &= 7432 \frac{\text{K}}{\text{W}} \end{aligned} \quad (5)$$

The radiation occurs in parallel with convection and conduction and is large relative to either of these resistances, therefore it is probably negligible.